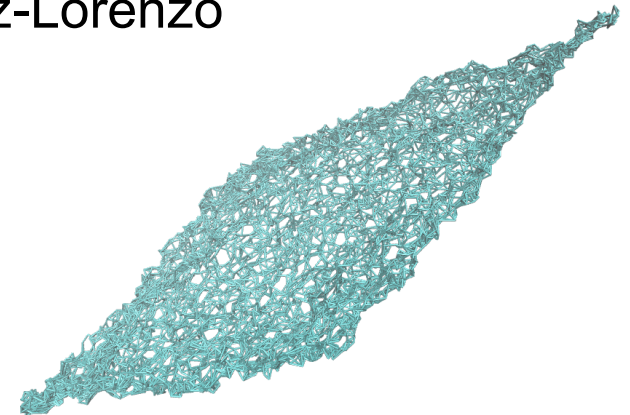
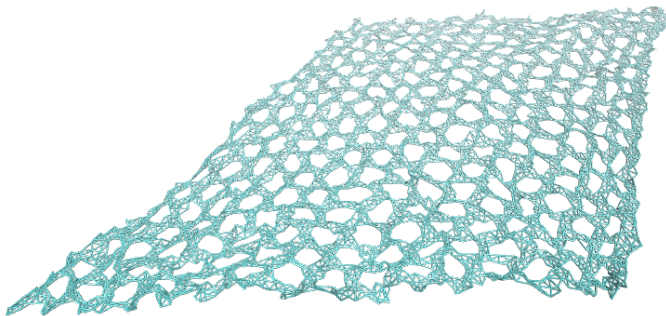


Crumpling Transition and Low Temperatures Properties of Crystalline Membranes with Perforation Patterns

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Overview

1 - Introduction

- Motivation
- Analytic definitions

2 - Methodology

- Simulations
- Analysis

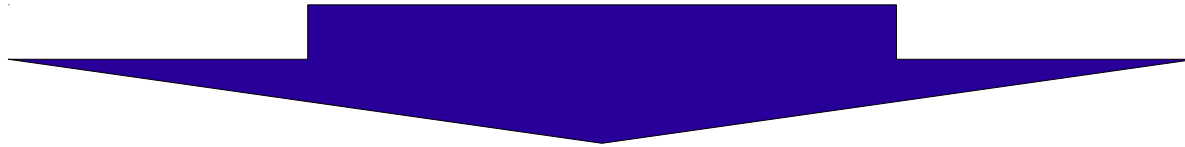
3 - Results

- Pure model: just to remind
- Perforated models: critical behavior
- Perforated models: flat phase elasticity

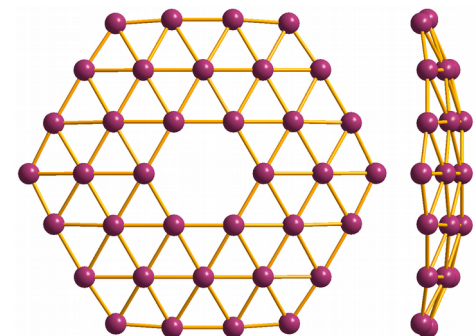
4 - Conclusions

Motivation

- We can define two main types of membranes:
 - Fluid membranes: variable topology.
 - Crystalline membranes: fixed connectivity.



- Characteristics
 - Transition between plane and crumpled phases
 - Negative Poisson module
- Examples:
 - Red blood cells skeleton
 - Graphite oxide thin sheets
 - Some 2D materials



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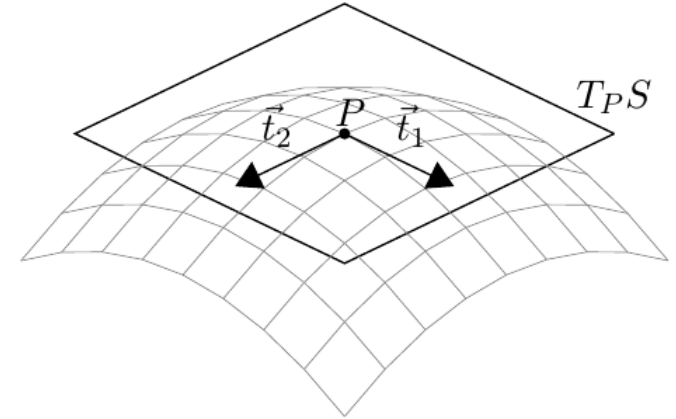
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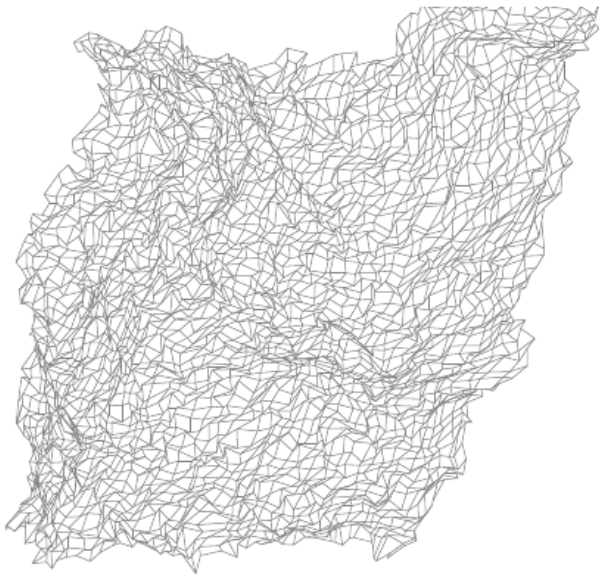
4 - Conclusions

Order parameter

- From the tangent vectors we can define the order parameter.

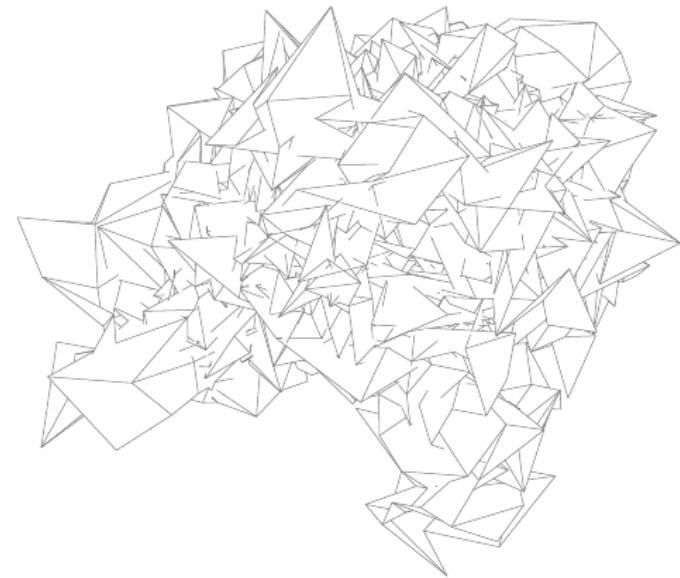


- Plane phase:



$$\langle \vec{t}_\alpha \rangle \neq 0$$

- Crumpled phase:



$$\langle \vec{t}_\alpha \rangle = 0$$

Free energy definition

- By imposing:
 - Locality, translational invariance.
 - Rotational and translational symmetry.
 - Self avoidance.

we can define the free energy as a sum of three terms:

$$F[\vec{t}_\alpha(\mathbf{x}), T] = F_E[\vec{t}_\alpha(\mathbf{x}), T] + F_C[\vec{t}_\alpha(\mathbf{x}), T] + F_b[\vec{t}_\alpha(\mathbf{x}), T]$$

with:

$$F_E[\vec{t}_\alpha(\mathbf{x}), T] = \int d^2\mathbf{s} \left[\frac{t}{2}(\vec{t}_\alpha \cdot \vec{t}^\alpha) + u(\vec{t}_\alpha \cdot \vec{t}_\beta)(\vec{t}^\alpha \cdot \vec{t}^\beta) + v(\vec{t}_\alpha \cdot \vec{t}^\alpha)(\vec{t}_\beta \cdot \vec{t}^\beta) \right]$$

$$F_C[\vec{t}_\alpha(\mathbf{x}), T] = \frac{\kappa}{2} \int d^2\mathbf{s} \partial_\alpha \vec{t}^\alpha \cdot \partial^\beta \vec{t}_\beta$$

$$F_b[\vec{t}_\alpha(\mathbf{x}), T] = \frac{b}{2} \int d^2\mathbf{x} d^2\mathbf{x}' \delta^2(\vec{r}(\mathbf{x}) - \vec{r}(\mathbf{x}')) \leftarrow \text{Not present if we use phantom surfaces}$$

Plane phase

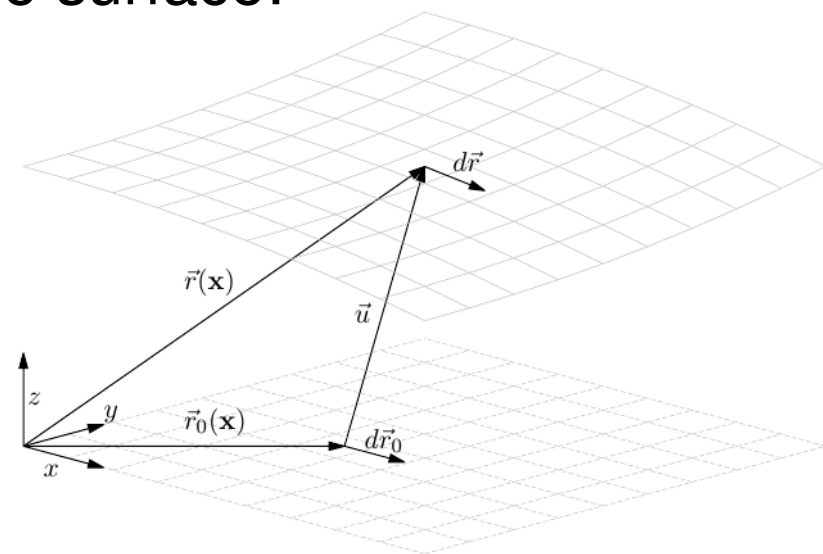
- From the Monge representation of the surface:

$$\vec{r}(\mathbf{x}) = (\mathbf{x} + \mathbf{u}(\mathbf{x}), h(\mathbf{x}))$$

$$(d\vec{r})^2 = (d\vec{r}_0)^2 + 2u_{\alpha\beta}dx^\alpha dx^\beta$$

being $u_{\alpha\beta}$ the deformation tensor:

$$u_{\alpha\beta} = \frac{1}{2}(\vec{t}_\alpha \cdot \vec{t}_\beta - \delta_{\alpha\beta}) \Rightarrow \vec{t}_\alpha \cdot \vec{t}_\beta = \delta_{\alpha\beta} + 2u_{\alpha\beta}$$



- Therefore:

$$F_E[u_{\alpha\beta}, T] = \int d^2\mathbf{x} \left[\mu u_{\alpha\beta} u^{\alpha\beta} + \frac{\lambda}{2} u_\alpha^\alpha u_\beta^\beta \right],$$
$$F_C[\mathbf{y}, T] \simeq \frac{\kappa}{2} \int d^2\mathbf{y} K_\alpha^\beta K^\alpha_\beta \simeq \frac{1}{2} \hat{\kappa} \int d^2\mathbf{y} H^2$$

Curvature tensor

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Discrete Pure Model

- 2D triangular lattice with $N=L^2$ points “living” in a 3D space
- Free boundary conditions
- Effective hamiltonian:

$$\mathcal{H} = \mathcal{H}_E + \mathcal{H}_C$$

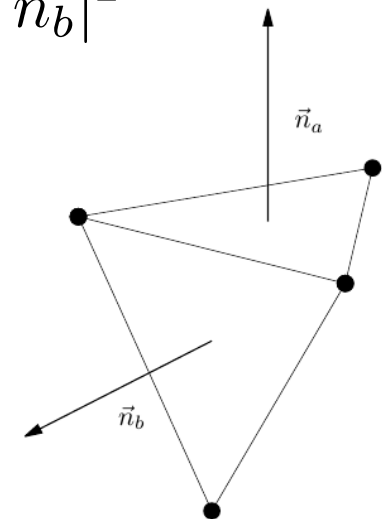
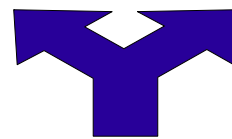
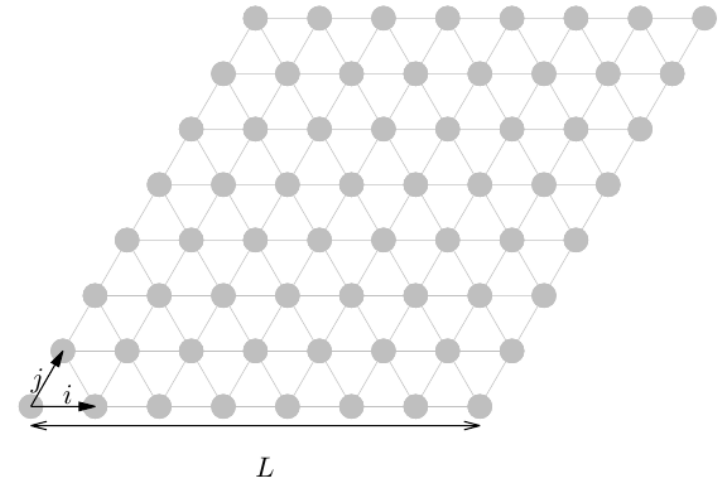
with:

$$\mathcal{H}_E = \frac{1}{2} \sum_{\langle ij \rangle} |\vec{r}_i - \vec{r}_j|^2$$

Elastic energy

$$\mathcal{H}_C = \frac{\kappa}{2} \sum_{\langle ab \rangle} |\vec{n}_a - \vec{n}_b|^2$$

Curvature energy



Reproduce the previous free energy in the continuous limit

Update Algorithm (Metropolis)

■ For a fixed value of κ

1) Choose a point i

2) Set $\vec{r}_i \rightarrow \vec{r}_i + \vec{\epsilon}$, with $\vec{\epsilon}$ randomly chosen on a box of size δ (chosen dynamically for acceptance $\sim 50\%$)

3) If $\Delta\mathcal{H} = \mathcal{H}_{NEW} - \mathcal{H}_{OLD} < 0$, accept the new position.

4) If $\Delta\mathcal{H} > 0$, accept the new position with probability $e^{-\Delta\mathcal{H}}$.

5) Repeat step 1 for every point in the lattice.

After enough iterations (thermalization): $P(\vec{r}_i) \propto e^{-\mathcal{H}(\kappa)}$

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Possible observable to extract

- Specific heat:

$$C_V = \frac{3(N-1)}{2} + \frac{\kappa^2}{N} (\langle E_C^2 \rangle - \langle E_C \rangle^2)$$

- Square of the gyration ratio

$$R_g^2 = \frac{1}{3N} \left\langle \sum_i \vec{R}_i \cdot \vec{R}_i \right\rangle = \frac{1}{3N} (\langle \vec{R}^2 \rangle - \langle \vec{R} \rangle^2), \quad \text{with} \quad \vec{R}_i = \vec{r}_{CM} - \vec{r}_i$$

- Gyration ratio kappa-derivative

$$\frac{\partial R_g^2}{\partial \kappa} = \langle R_g^2 E_C \rangle - \langle R_g^2 \rangle \langle E_C \rangle \equiv \langle R_g^2 E_C \rangle_c = N \langle R_g^2 e_C \rangle_c,$$

- Poisson Module

$$\sigma = -\frac{\delta x^2 / x^2}{\delta x^1 / x^1} \quad \begin{array}{l} \text{Compression and shear modules} \\ \swarrow \quad \searrow \\ \sigma = \frac{K - \mu}{K + \mu} \end{array} = -\frac{\langle u_{11} u_{22} \rangle_c}{\langle u_{22}^2 \rangle_c} = -\frac{\langle g_{11} g_{22} \rangle_c}{\langle g_{22}^2 \rangle_c} \quad \begin{array}{l} \text{Induced metric tensor} \\ \swarrow \\ g_{\alpha\beta} = \vec{t}_\alpha \cdot \vec{t}_\beta \end{array}$$

Finite Size Scaling and kappa extrapolations

- We can obtain critical exponents via standard FSS with κ playing the role of (inverse) temperature.

- For a given observable:

$$\mathcal{O}_L \sim L^{\frac{x_0}{\nu}} f [L(\kappa(L) - \kappa_c(\infty))^\nu]$$

- In the maximum of the observable:

- We obtain the critical exponent by: $\mathcal{O}_L^{max} \sim L^{\frac{x_0}{\nu}}$

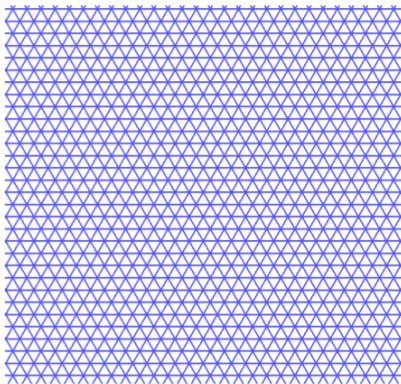
- We can also use: $\kappa_c(L) = \kappa_c(\infty) + x_C L^{1/\nu}$

- We can locate the maximum using extrapolations in κ :

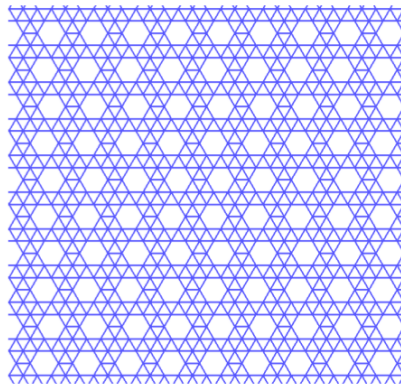
$$\langle O \rangle_{\kappa'} = \frac{\sum_E O(E) p_\kappa(E) e^{-(\kappa' - \kappa) E_c}}{\sum_E e^{-(\kappa' - \kappa) E_c}} \quad \leftarrow \text{Curvature energy}$$

What does it happen if we perforate the model?

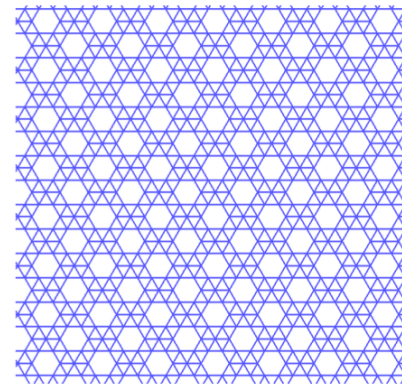
- Following: *D. Yllanes, S. Bhabesh, D.R.Nelson & M.J. Bowick, Nature Communications 8, 1381 (2017)*
- We can define patterns of perforations spanning all the lattice.
 - Different sizes ($R=1$ or 2), distances, and shifts.



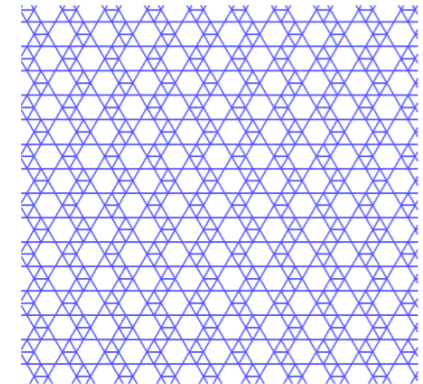
Full membrane



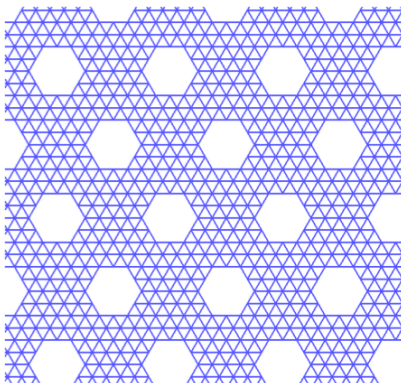
Pattern 1



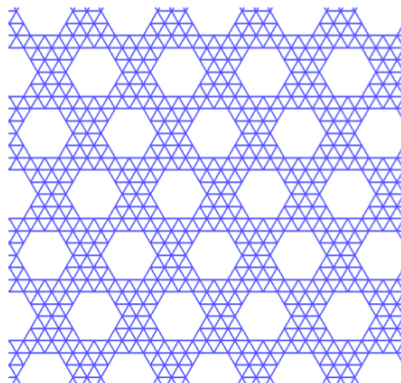
Pattern 2



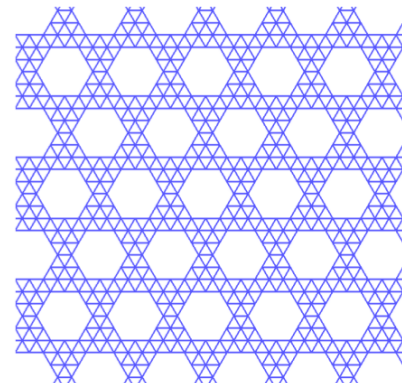
Pattern 3



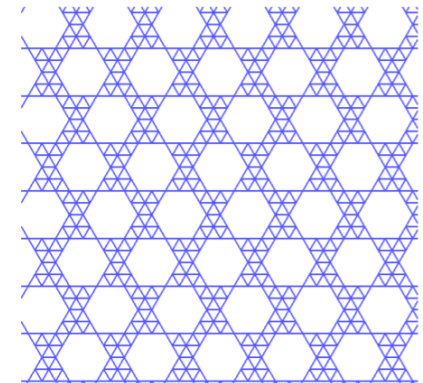
Pattern A



Pattern B



Pattern C



Pattern D

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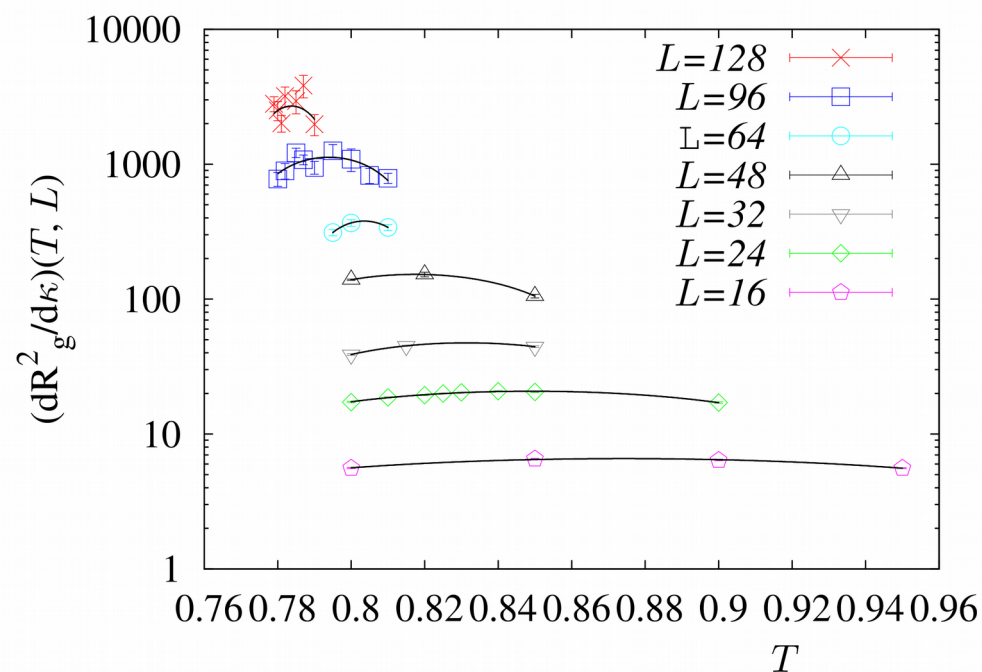
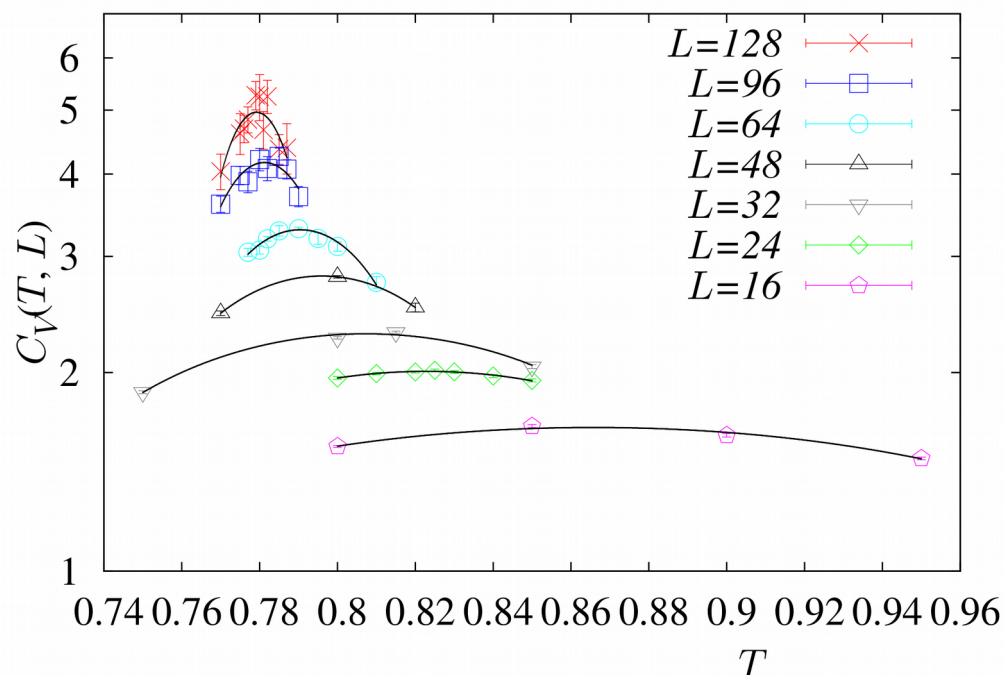
Pure model: just to remind

- We simulated systems with $16 \leq L \leq 128$, focusing around

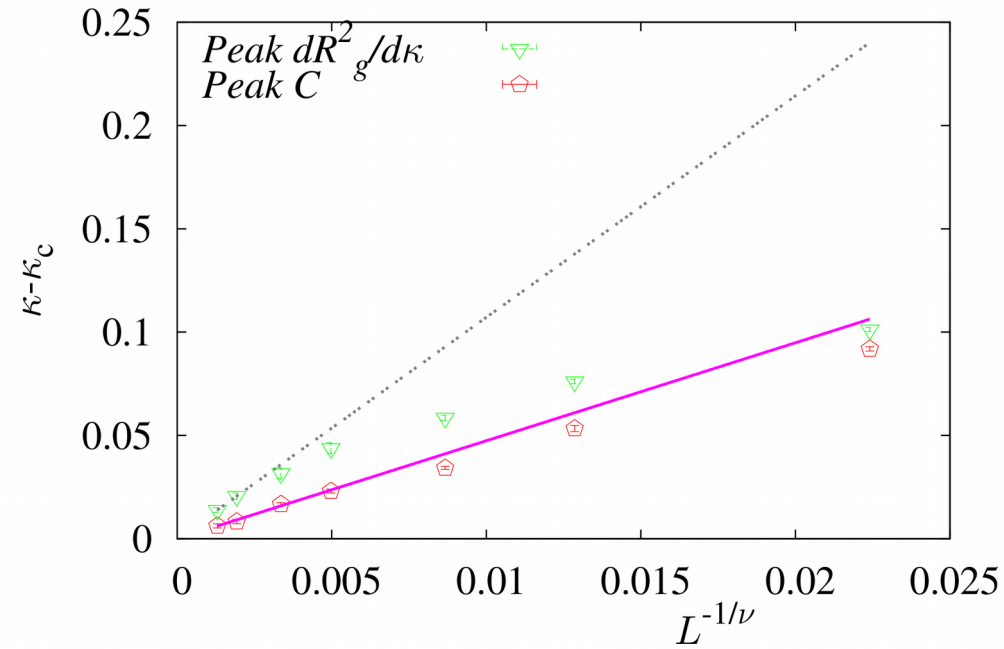
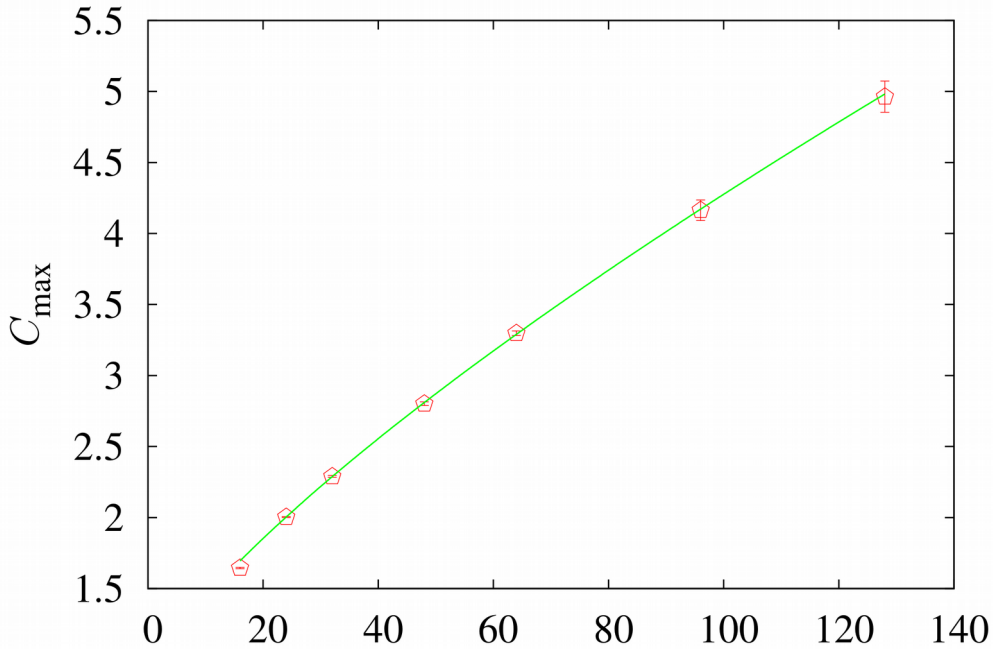
$$0.5 \leq \kappa \leq 2 \quad \kappa_c \approx 0.8$$

- We checked that the behavior is critical and were able to distinguish between discrepancies in previous works.

Phys. Rev. E 93, 022111 (2016). arXiv:1511.08615



Pure model: critical behavior



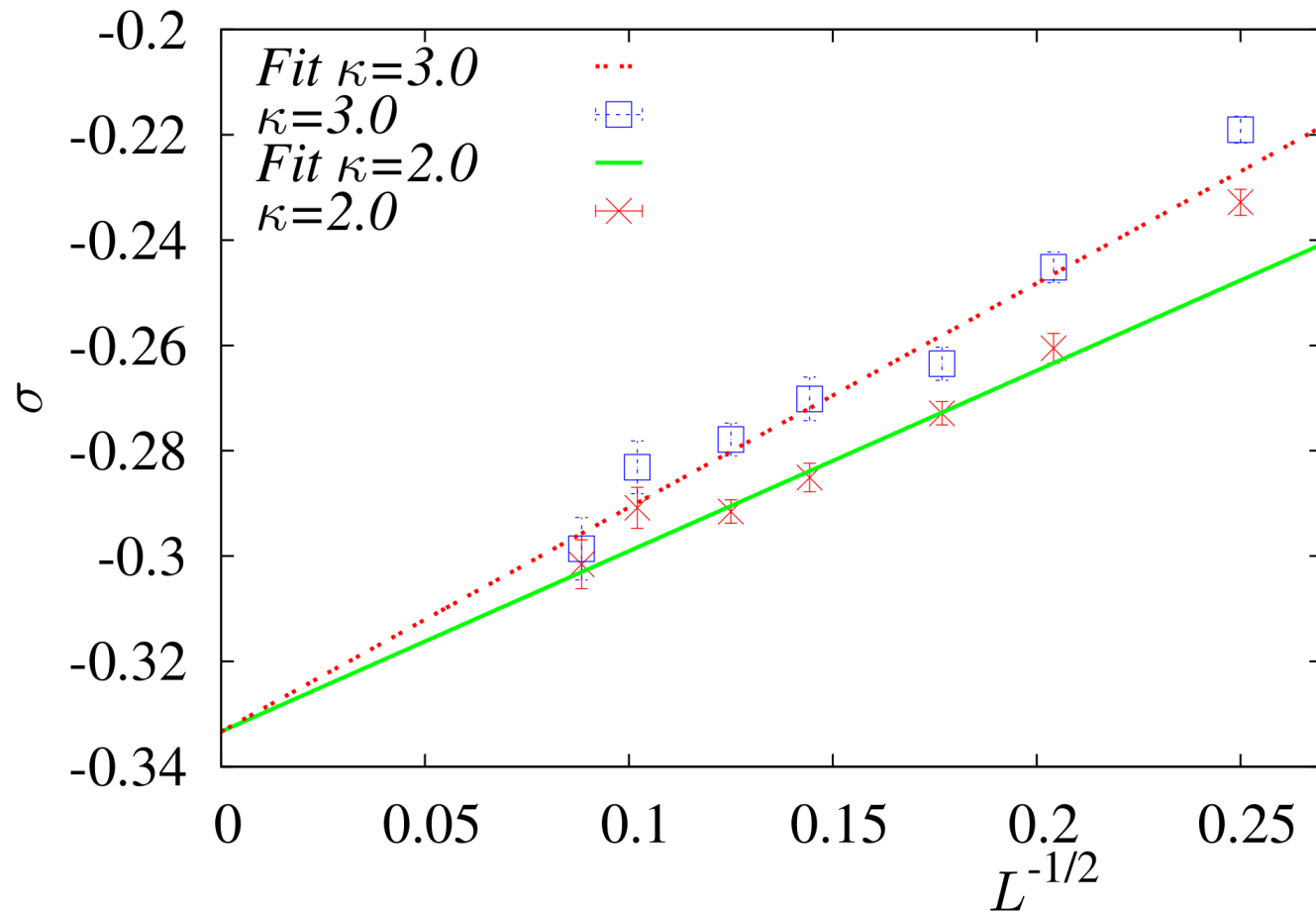
$$\kappa_c(L) = \kappa_c(\infty) + C_0 L^{-1/\nu}, \quad \kappa_c(\infty) = 0.777(3)(3)$$

Coefficients/Critical Exponents	Results
c_0	0.7702(36)
c_1	0.1098(95)
$c_2 = \alpha/\nu$	0.76(18)
α	0.55(18)
ν	0.72(4)
χ_c^2/ndf	0.38/2
$P(\chi^2 > \chi_c^2)$	0.8257

Good agreement with previous estimations

Quite precise compared with previous estimations

Pure model: Poisson module at low temperature (flat phase)



Both s_1 and s_2 extrapolate well to the analytical value -0.33 , with the expected power law.

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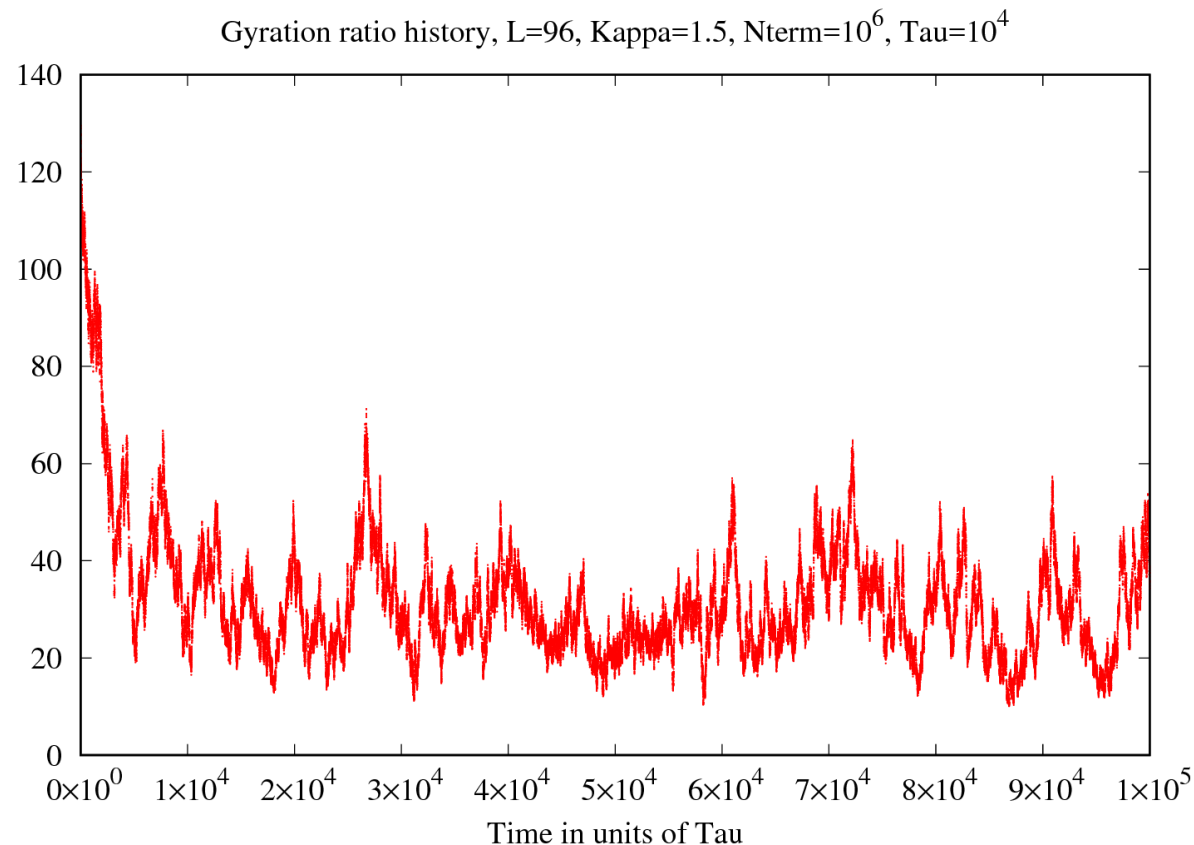
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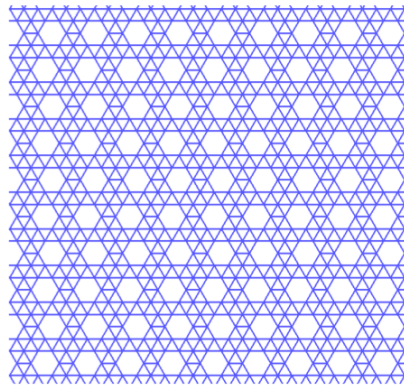
Thermalization

- These surfaces can have a more slow behavior and longer correlation times.
- Take care with thermalization steps and frequency of measures (we use 10^7 and 10^5 MC full sweeps, respectively).

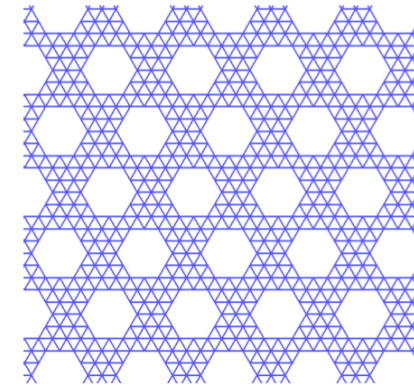


Perforated models: critical behavior

- We have checked it with the patterns:



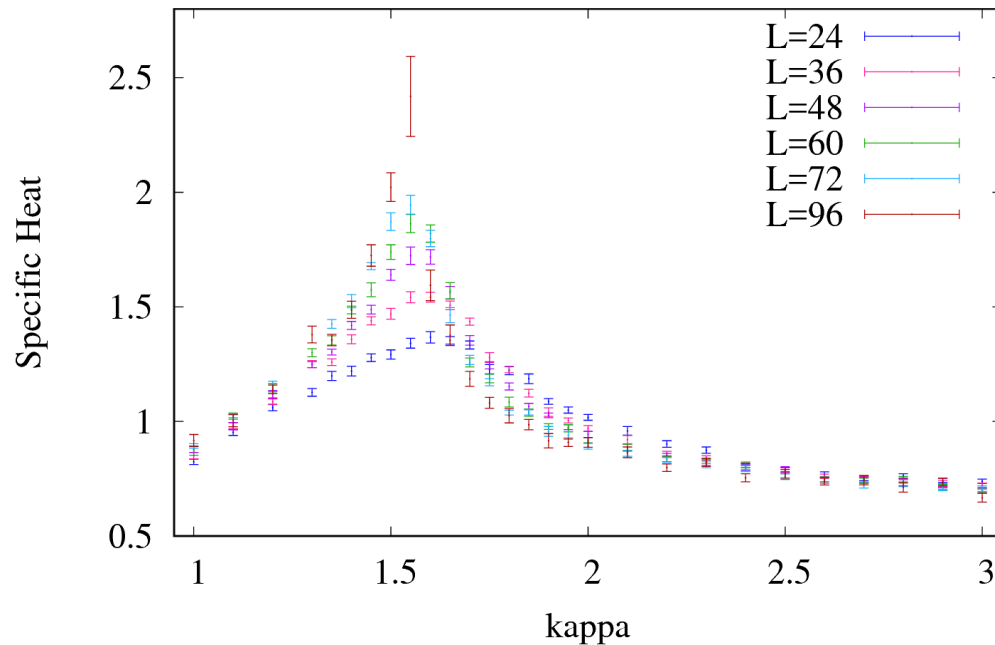
Pattern 1



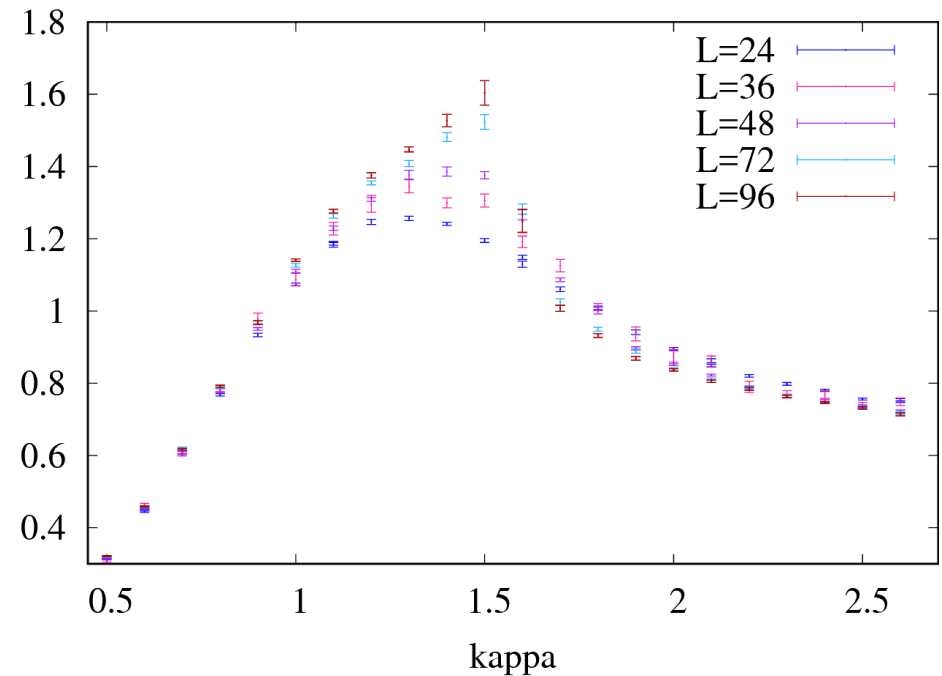
Pattern B

They have very similar K_c

Specific heat VS kappa, Pattern 1

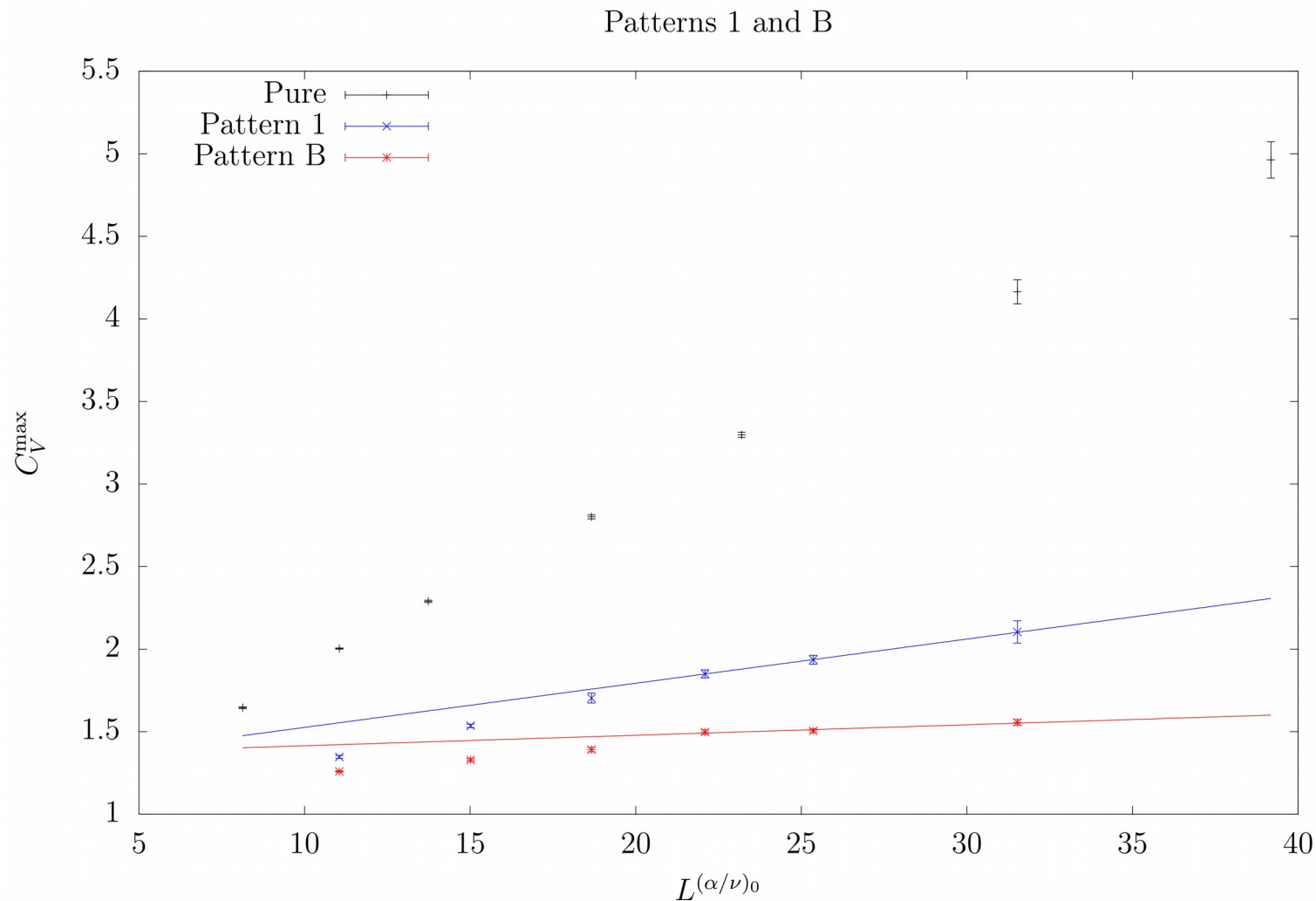


Specific heat VS kappa, Pattern B



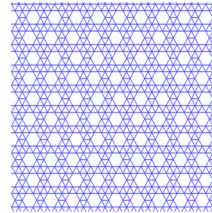
Perforated models: critical behavior

- We can check with both signals good compatibility with the critical exponents of the pure model .

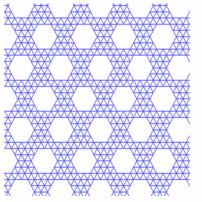


Perforated models: critical behavior

- We can also use the signal from the gyration ratio kappa-derivative:

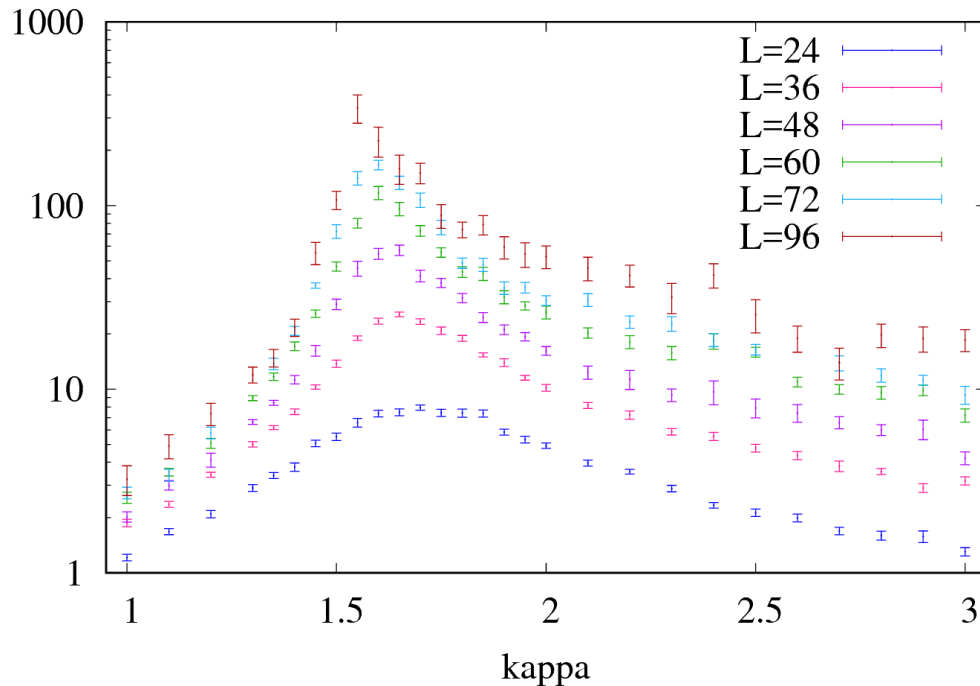


Pattern 1

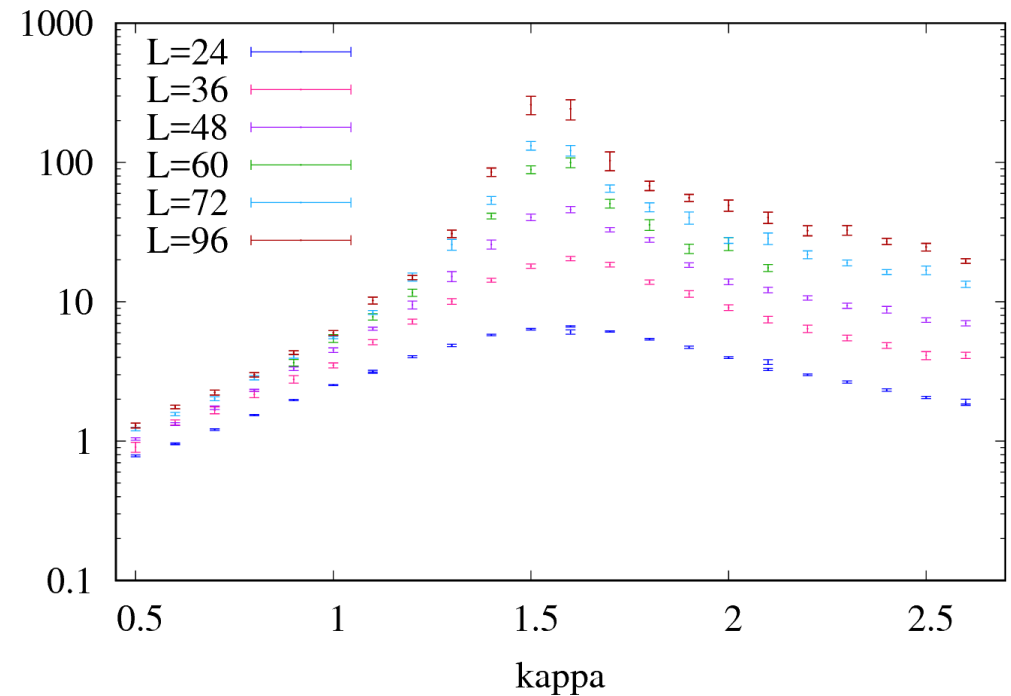


Pattern B

Gyration ratio kappa-derivative VS kappa, Pattern 1

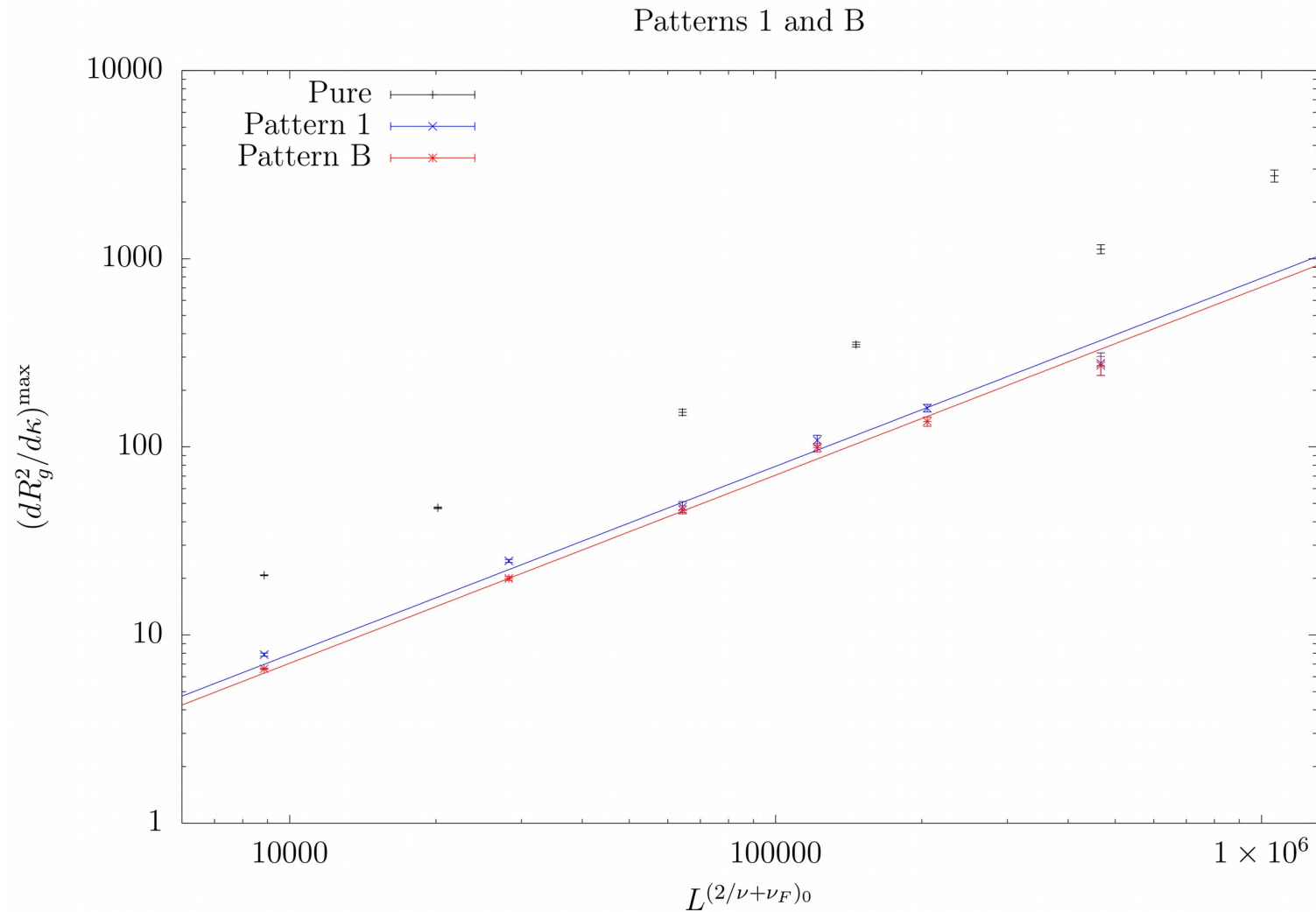


Gyration ratio kappa-derivative VS kappa, Pattern B



Perforated models: critical behavior

- Again, we can check with both signals the compatibility with the critical exponents of the pure model .



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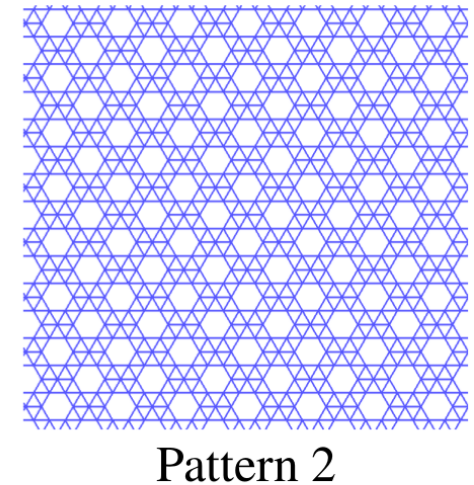
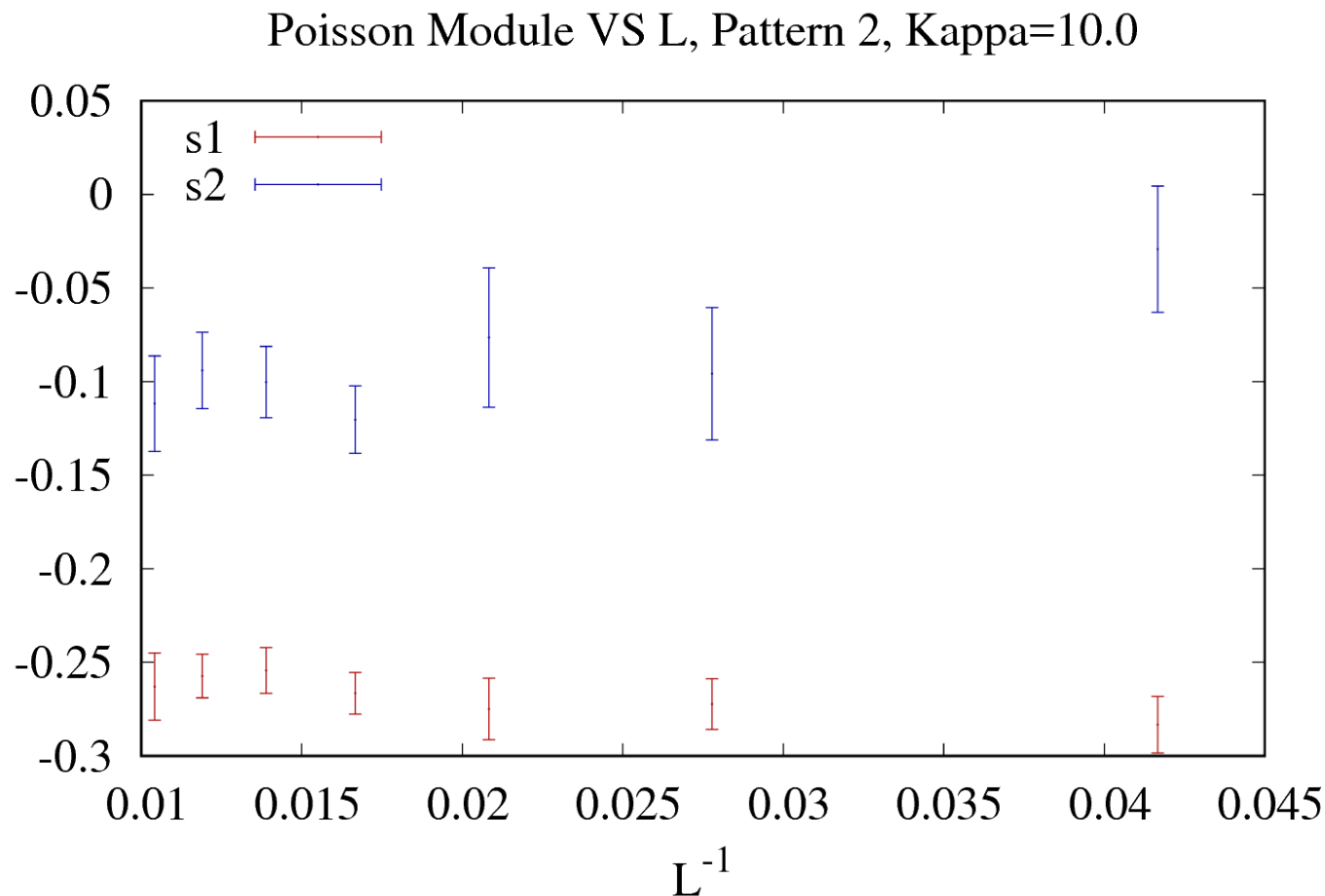
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Perforated models: flat phase elasticity

- In the perforated cases, we have now anisotropy, which is also evidenced by the differences in s_1 and s_2



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Conclusions

- Following D. Yllanes, et al. (*Nature Communications* 8, 1381 (2017)), we are studying crystalline membranes using MC simulations with different patterns of perforations.
- Good agreement with the pure model for critical exponents.
Disagreement with the Poisson Module (anisotropy).
- There is still quite room for numerical improvement.
- Model easily tunable. Possible next steps:
 - insert a fixed substrate and look the adhesion properties
 - insert another neighbor surface and interactions
 - simulate tubes instead of plane surfaces...

Thank you for your attention.