Dissipative Dynamics of a Single Polymer: An explicit solvent framework with Lowe-Andersen approach

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Introduction



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Introduction



Collapse Transition: Relevant for conformational transition of macromolecules in general

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Phenomenological Models on Collapse Kinetics

Phenomenological Models on Collapse Kinetics



Hydrodynamic Dissipation of surface energy



Phenomenological Models on Collapse Kinetics



Hydrodynamic Dissipation of surface energy



pear necklace model: Formation of nascent clusters followed by coarsening of clusters to form bigger clusters and eventually a single globule

A. Halperin and P.M. Goldbart, Phys. Rev. E 61, 565 (2000)

Available Simulations Results

- Monte Carlo Simulations of both lattice and off-lattice models produce the "pearl-necklace" picture
- Molecular dynamics simulations both with implicit and explicit solvent molecules yield the same phenomenological picture.
- Even relatively recent result using Dissipative Particle Dynamics (DPD) reproduces the same picture
- Although in each of these cases the overall collapse-time scalings are different depending on whether hydrodynamics is preserved or not.

Idea: Rather than changing only the qualilty of the solvent from good to poor, one can also think about other general properties of the solvent that control energy dissipation, e.g., viscosity.

The Model

Bonded potential:
$$V_{\text{FENE}}(r) = -\frac{\kappa}{2}R^2 \ln (1 - [(r - r_0)/R]^2);$$

 $r_0 = 0.7, R = 0.3, \text{ and } K = 40$

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The Model

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Non-Bonded intercation:

Both for polymer and solvent beads

$$V_{\rm LJ}^*(r) = \begin{cases} V_{\rm LJ}(r) - V_{\rm LJ}(r_c) & r < r_c \\ 0 & \text{else} \end{cases}$$

$$V_{
m LJ}(r)=4\epsilon\left[(\sigma/r)^{12}-(\sigma/r)^6
ight]$$
, where $\sigma=r_0/2^{1/6}$

good solvent: $r_c = 2^{1/6}\sigma$ for sol-sol,sol-mon,mon-mon poor solvent: $r_c = 2^{1/6}\sigma$ for sol-sol,sol-mon and $r_c = 2.5\sigma$ for mon-mon

Explicit Solvent Model

Factors taken into account

- In reality, while a polymer moves in a solvent experiences friction
- Thereby, the disspation of energy is dependent on the viscosity of the solvent

• Preservation of hydrodynamics (is what makes a fluid fluid)

Possible Ways

- Langevin Dynamics (Mesoscopic)
- Brownian Dynamics
- Dissipative Particle Dynamics

Construction of an Explicit Solvent Model

Langevin Equation:

 $m\frac{d^2\vec{r}}{dt^2} = -\gamma\frac{d\vec{r}}{dt} + \vec{F_R} + \vec{F_C}$

 γ is the friction coffiecient

 $\vec{F_R}$ is a random force that accounts for thermal fluctuations such that $\langle \vec{F_R}(t) \vec{F_R}(t') \rangle = \sqrt{2kT\gamma} \delta(t-t')$ and $\langle \vec{F_R}(t) \rangle = 0$

 $\vec{F_C}$ conservative forces due to particle particle intercation

Disadvantages: Only thermal fluctuation but no hydrodynamics. Also one cannot use large dt.

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Construction of an Explicit Solvent Model

Brownian Dynamics:

Neglect the inertial term in the Langevin equation and solve the corresponding Smoluchowski equation. As such, only particle positions enter

 $\frac{d\vec{r}}{dt} = \vec{F_C}D/kT + \vec{F_R}(t)/\gamma$ implies the for a particle *i*, $\vec{r_i}(t + \Delta t) = \vec{r_i}(t) + \Delta t \sum_j \frac{\mu \vec{i_j} \cdot \vec{F_c}}{kT} + \delta \vec{F_R}$

 $\vec{\mu}_{ij}$ is the mobility tensor If $\vec{\mu}_{ij} = 0$ for $i \neq j$ then no HI

Introducing HI is cumbersome as one has to consider pairwise terms considering Oseen tensor

A.J. Banchio and J.F. Brady J. Chem. Phys. 118, 10323 (2003)

P.J. Hoogerbrugge and J.M.V.A. Koelman, Europhys. Lett. **19**, 155 (1992) J.M.V.A. Koelman and P.J. Hoogerbrugge and , Europhys. Lett. **21**, 363 (1993)

The formulation usually used now is due to Espanol and Warren P. Espanol and P.B. Warren, Europhys. Lett. **30**, 191, (1995).

Newton's equation of motion:

$$rac{dec{r}}{dt}=ec{v}_i ext{ and } rac{dec{p}_i}{dt}=ec{f}_i$$
 $ec{f}_i=ec{F_C}+ec{F_R}+ec{F_D}$

 $\vec{F_C}$: Conservative forces, i.e., due to intercation between particles $\vec{F_R}$: Random forces, i.e., due to thermal fluctuations $\vec{F_D}$: Nonconservative or Dissipative forces



$$\vec{F_D} = \vec{f_{ij}} = -\gamma w_d(r_{ij})(\vec{r_{ij}}.\vec{v_{ij}})\vec{r_{ij}}$$

 $\vec{r_{ij}} = \vec{r_i} - \vec{r_j}$ and $\vec{v_{ij}} = \vec{v_i} - \vec{v_j}$
Component of relative velocity along line of
centres

 $w_d(r_{ij})$ is weight function that is zero for $r_{ij} > r_c$

$$\vec{F_R} = \vec{f_{ij}^R} = Aw_r(r_{ij})\theta_{ij}\vec{r_{ij}}$$

A: Noise Amplitude

 θ_{ij} is Gaussian distributed with zero mean and unit variance $w_r(r_{ij})$ is weight function that is zero for $r_{ij} > r_c$

To have the correct canonical distribution function (constant NVT) the dissipative (cools the system) and random (heats the system) forces are related:

$$w_d(r_{ij}) = [w_r(r_{ij})]^2$$
 and $A^2 = 2\gamma kT$

Popular form of the weigth function:

$$w_d(r_{ij}) = \left(1 - \frac{r_{ij}}{r_c}\right)$$

Advantages

- Without F_D and F_R it is simply molecular dynamics
- Provides a canonical distribution hence can act as thermostat for any conservative soft potential
- It is local, conserves momenta and Galilean invarient. Hence, hydrodynamics is preserved
- It is possible to tune the viscosity of the medium by varying γ in F_D

Disadvantages

- Solving the DPD equations of motion is an issue because of the velocity dependent F_D
- *dt* needs to be much small to minimize the error hence computationally expensive

Our Approach: Lowe-Andersen

C.P. Lowe, Europhys. Lett., 47, 145 (1999)

In the spirit of Andersen thermostat:

- Using relative velocities instead of velocities
- Collisions exchange relative momentum between pair of particles by taking a new relative velocity from the Maxwellian distribution for relative velocities

- Component of relative velocity along line of centres like in DPD
- detail balance is satisfied along with momenta conservation

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Lowe-Andersen Approach



 $\vec{v}_i \leftarrow \vec{v}_i + \frac{1}{2} \frac{1}{m} \vec{F}_i^C \Delta t$

$$\vec{r}_i \leftarrow \vec{r}_i + \vec{v}_i \Delta t$$

Calculate
$$\vec{F}_i^C \{\vec{r}_j\}$$

$$\vec{v}_i \leftarrow \vec{v}_i + \frac{1}{2} \frac{1}{m} F_i^C \Delta t$$

For all pairs of particles for which $r_{ij} < r_c$

(i) Generate $\vec{v}_{ij}^{\circ} \cdot \vec{e}_{ij}$ from a distribution $\xi_{ij}^{(g)} \sqrt{2k_B T^*/m}$ (ii) $2\vec{\Delta}_{ij} = \vec{e}_{ij} (\vec{v}_{ij}^{\circ} - \vec{v}_{ij}) \cdot \vec{e}_{ij}$ (iii) $\vec{v}_i \leftarrow \vec{v}_i + \vec{\Delta}_{ij}$ (iv) $\vec{v}_j \leftarrow \vec{v}_j - \vec{\Delta}_{ij}$ with probability $\Gamma \Delta t$

Calculate physical quantities

Simulation details:

cubic box of size $L = 1.25 N^{3/5}$, N is the no. of monomers

Density of the solvent beads ho = 0.7 r_c for the thermostat = r_c for good solvent = $2^{1/6}\sigma$

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Equilibrium Static Properties in Good Solvent

Radius of Gyration:



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Trajectory of the the centre of mass of a polymer

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$$MSD = \left\langle [\vec{R_{cm}(t)} - \vec{R_{cm}(t_0)}]^2 \right\rangle$$



ballistic regime: $MSD \sim t^2$ diffusive regime: MSD = 6Dt (Einstein Equation in 3-d) where *D* is the diffusion constant for the CM of the polymer

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Zimm's scaling: $D \sim N^{0.6}$

valid for hydrodynamic intercations

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