

# Aggregation of semiflexible polymers under constraints

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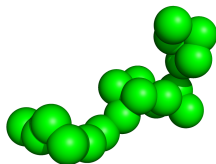
Institut für Theoretische Physik  
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27.11.2014



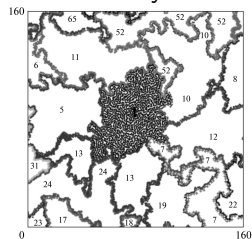
## Setting the scope

single



isolated

many

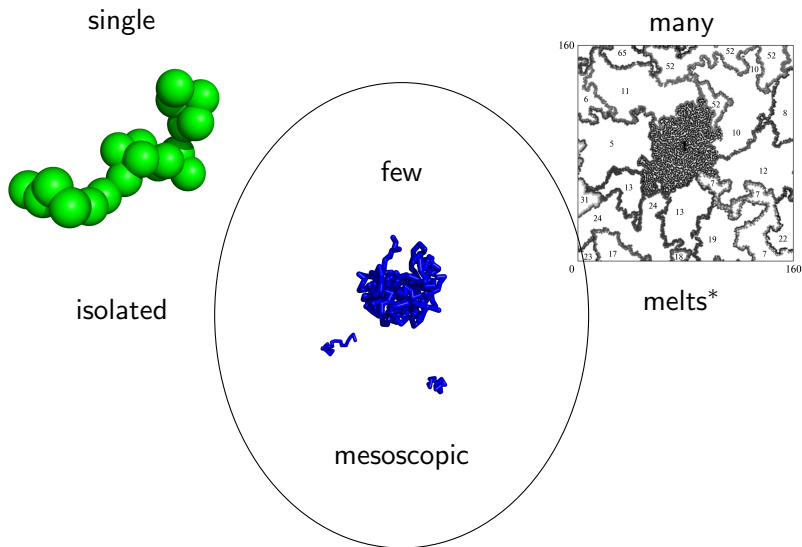


melts\*

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\* taken from Schulmann et al., Polymer Science **55**, 181 (2013).

# Setting the scope

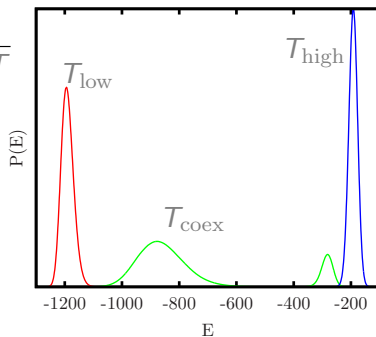


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# Method: Multicanonical Markov Chain Monte Carlo<sup>1</sup>

Attempt to cover full temperature range with a single simulation.

$$Z_{\text{can}} = \sum_E \Omega(E) e^{-\beta E}, \quad \beta = \frac{1}{k_B T}$$



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<sup>1</sup>B. A. Berg and T. Neuhaus, Phys. Lett. B **267** 249 (1991), Phys. Rev. Lett. **68** 9 (1992).

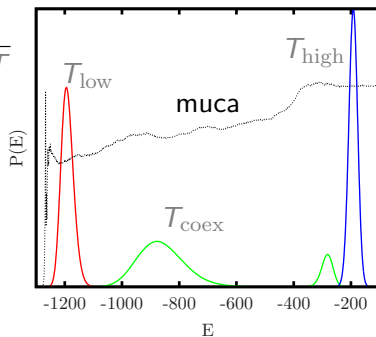
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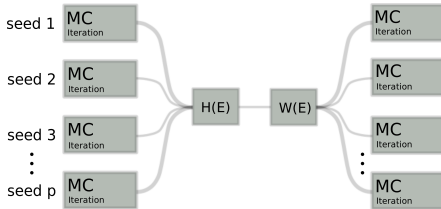
$$Z_{\text{muca}} = \sum_E \Omega(E) W(E)$$



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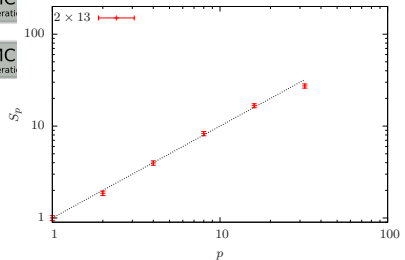
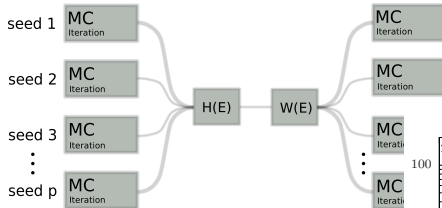
# Parallel MUCA<sup>2</sup>

Distribute the time-consuming iteration process onto independent Markov Chains

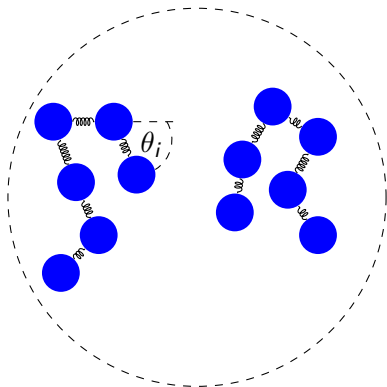


# Parallel MUCA<sup>2</sup>

Distribute the time-consuming iteration process onto independent Markov Chains



# Semiflexible Homopolymers



Energy contributions:

- non-bonded (LJ):

$$\sum_{i,j} 4\epsilon \left( \left( \frac{\sigma}{r_{ij}} \right)^{12} - \left( \frac{\sigma}{r_{ij}} \right)^6 \right)$$

- bonded (FENE):

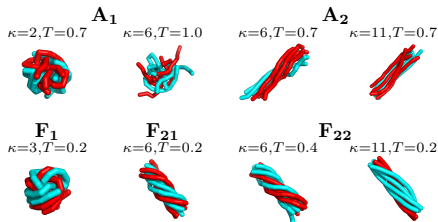
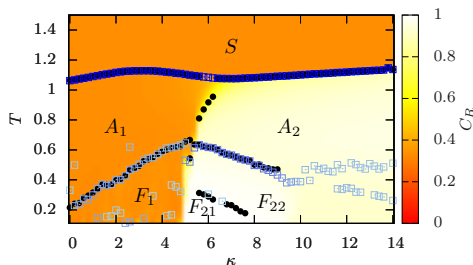
$$\sum_i -\frac{\kappa}{2} R^2 \ln \left( 1 - \left( \frac{r_{i,i+1} - r_0}{R} \right)^2 \right)$$

- bending (WLC):

$$\sum_i \kappa (1 - \cos \theta_i)$$



# Effect of Stiffness for 8 polymers ( $N = 13$ )<sup>3</sup>



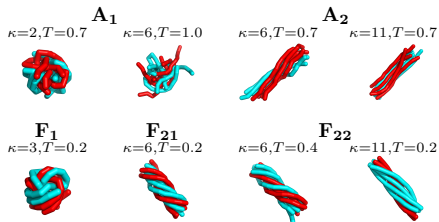
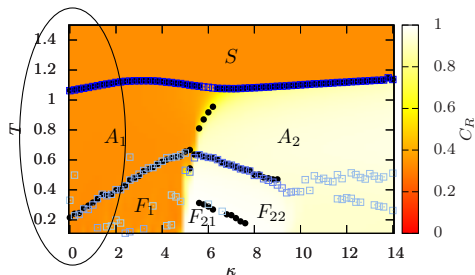
$$C_R = \frac{2}{M(M-1)} \sum_{i < j} (\hat{\mathbf{R}}_i \hat{\mathbf{R}}_j)^2$$

Structural motifs range from amorphous aggregates to polymer bundles.

$$\rho = MN/L^3 = 0.001$$

<sup>3</sup>J.Z. and W. Janke, submitted (2014).

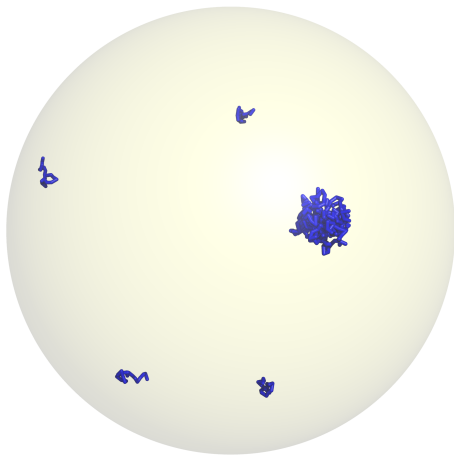
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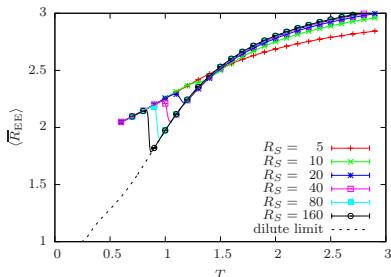
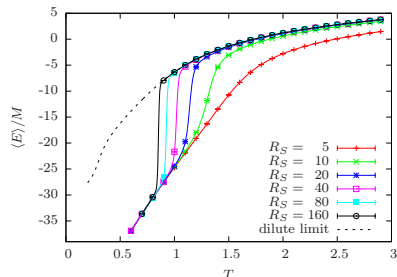
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# Isolated Chain approximation<sup>4</sup>

Flexible ( $\kappa = 0, 8 \times 13$ ):



$R_S \rightarrow \infty$ : isolated chain approximation for  $T = 0$ .

volume fraction of multi-polymer system:  $\Phi = NM \left(\frac{r_0}{2}\right)^3 / R_S^3$

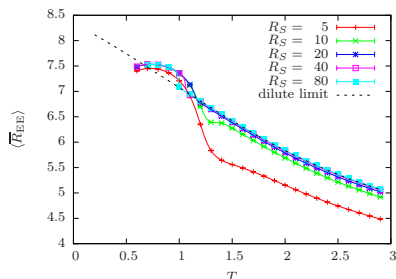
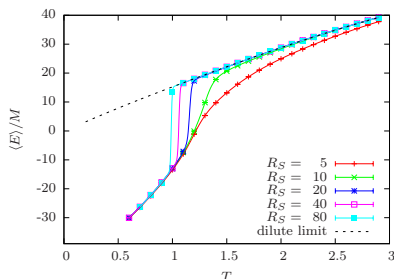
intrinsic volume fraction of single coil:  $\Phi^* \simeq \frac{N \left(\frac{r_0}{2}\right)^3}{R_{EE}^3}$ ,  $R_{EE} \simeq r_0 N^\nu$

semi-dilute:  $R_S^c \simeq r_0 M^{1/3} N^\nu \approx 6.3$

<sup>4</sup>J.Z., M. Mueller, P. Schierz, M. Marenz, and W. Janke, J. Chem. Phys **141**, 114908 (2014).

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Stiff ( $\kappa = 9, 8 \times 13$ ):



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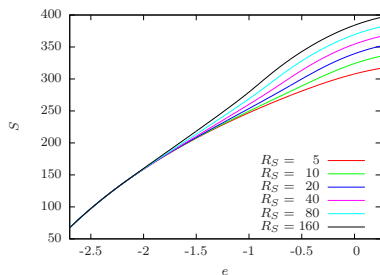
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# Relation between aggregation temperature and density<sup>4</sup>



Gibbs Construction:

$$\beta_{\text{agg}} = \frac{S(E_{\text{sep}}) - S(E_{\text{agg}})}{\Delta E}.$$

Ideal gas approximation:

$$S(E_{\text{sep}}) \sim \ln \left[ \left( \frac{4\pi}{3} R_S^3 \right)^M \right] \propto M \ln R_S$$

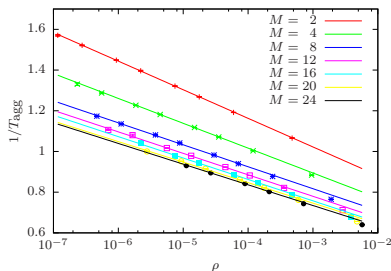
Assume  $\Delta E = M\Delta e$  and  $S(E_{\text{sep}}) \gg S(E_{\text{agg}})$

$$\beta_{\text{agg}}(R_S) \sim \ln R_S + \text{const} \sim -a_1 \ln \rho + a_2.^5$$

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## Finite-size corrections for $M^4$

Assume a large fraction of polymers in aggregate with

$$R_{\text{gyr}} \sim M^{1/3}.$$

Due to surface effects of aggregate, expect finite-size corrections of order  $R^{-1}$

$$T_{\text{agg}}(M, \rho) \propto \left( 1 + s(\rho)M^{-1/3} + \mathcal{O}\left(M^{-2/3}\right) \right),$$

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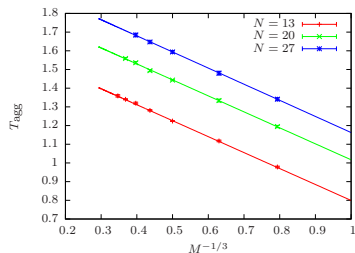


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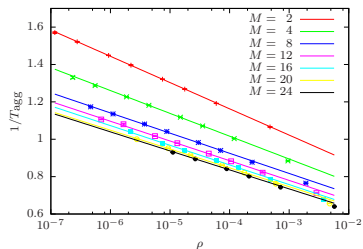
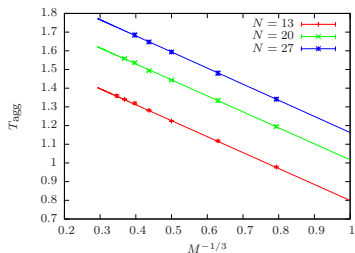


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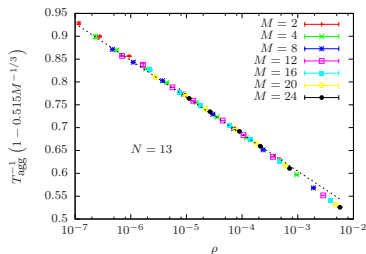
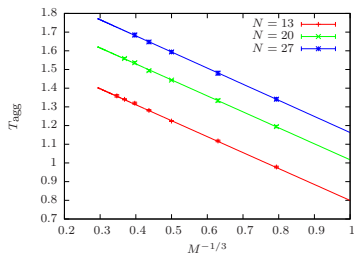


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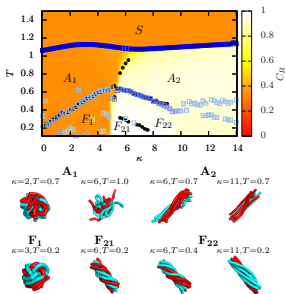
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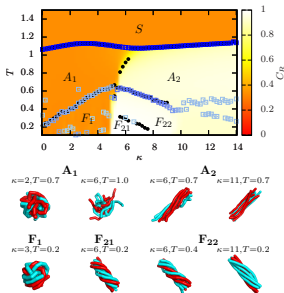
# Summary

- Key role of stiffness on polymer aggregation



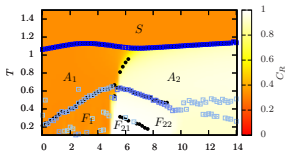
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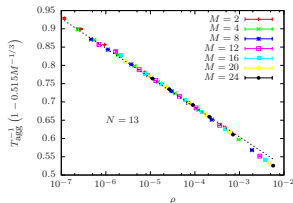
- Key role of stiffness on polymer aggregation
- Competition between collapse and aggregation yields lower temperature bound for isolated chain approximation
- General relation between aggregation temperature and density in the mesoscopic regime.



$\kappa=2, T=0.7$   $A_1$   $\kappa=6, T=1.0$   $\kappa=6, T=0.7$   $A_2$   $\kappa=11, T=0.7$



$\kappa=3, T=0.2$   $F_1$   $\kappa=6, T=0.2$   $F_{21}$   $\kappa=6, T=0.4$   $F_{22}$   $\kappa=11, T=0.2$



## Acknowledgments

# Thank you for your attention



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