



Controlling  
material  
properties

Christoph  
Junghans

# Controlling material properties using a thermostat

Christoph Junghans

Max Planck Institute for Polymer Research  
Mainz

Nov 30, 2007



# Outline

Controlling  
material  
properties

Christoph  
Junghans

- 1 Motivation
- 2 Introduction
- 3 DPD Thermostat
- 4 Simulations
- 5 Conclusion

# Motivation

Controlling  
material  
properties

Christoph  
Junghans

Motivation

Introduction

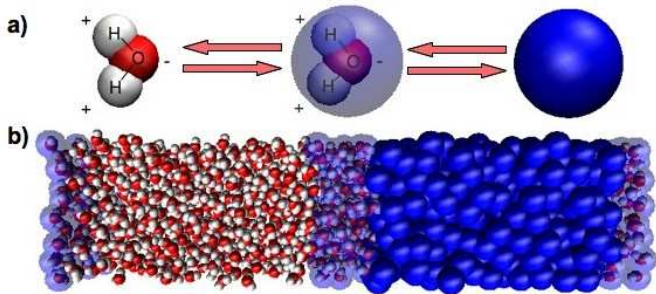
DPD  
Thermostat

Simulations

Conclusion

Changing of material properties is useful for:

- Fitting models to real experiments
- Multiscale simulations (AdResS, QMM, etc.)



1

<sup>1</sup>From: M. Praprotnik, S. Matysiak, L. Delle Site, K. Kremer and C. Clementi, J. Phys. Condens. Matter 19, 292201, 2007.



# Molecular Dynamics

NVE vs. NVT

Controlling  
material  
properties

Christoph  
Junghans

Motivation

Introduction

DPD  
Thermostat

Simulations

Conclusion

## Newton's Equation of Motion

$$m\ddot{\vec{r}}_i = \underbrace{\vec{F}_i}_{\text{Deterministic part}} + \underbrace{\vec{F}_i^D + \vec{F}_i^R}_{\text{Langevin Thermostat}}$$

+      +

Damping part      Random part

Ensemble: NVE



# Molecular Dynamics

NVE vs. NVT

Controlling  
material  
properties

Christoph  
Junghans

Motivation

Introduction

DPD  
Thermostat

Simulations

Conclusion

## Newton's Equation of Motion

$$m\ddot{\vec{r}}_i = \underbrace{\vec{F}_i}_{\text{Deterministic part}} + \underbrace{\vec{F}_i^D}_{\text{Damping part}} + \underbrace{\vec{F}_i^R}_{\text{Random part}}$$

Langevin Thermostat

Ensemble: NVT

## Advantages of DPD

- Local thermostat
- Galilei invariant
- Satisfies Newton III
- Conservation → Hydrodynamics
  - Mass
  - Momentum
  - Angular momentum
- Does not influence the dynamics very much

---

<sup>2</sup>T. Soddemann, B. Dünweg, and K. Kremer (2003)

# DPD Equations I

## Damping and random force

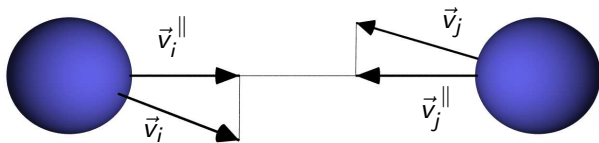
$$\vec{F}_i^D = \sum_{j \neq i} \vec{F}_{ij}^D \quad \text{and} \quad \vec{F}_i^R = \sum_{j \neq i} \vec{F}_{ij}^R$$

with

$$\vec{F}_{ij}^D = -\zeta(r_{ij})(\hat{r}_{ij} \otimes \hat{r}_{ij})\vec{v}_{ij}$$

and

$$\vec{F}_{ij}^R = \sigma(r_{ij})\hat{r}_{ij}\theta_{ij}$$



Controlling  
material  
properties

Christoph  
Junghans

Motivation

Introduction

DPD  
Thermostat

Simulations

Conclusion

# DPD Equations I

Controlling  
material  
properties

Christoph  
Junghans

Motivation

Introduction

DPD  
Thermostat

Simulations

Conclusion

## Damping and random force

$$\vec{F}_i^D = \sum_{j \neq i} \vec{F}_{ij}^D \quad \text{and} \quad \vec{F}_i^R = \sum_{j \neq i} \vec{F}_{ij}^R$$

with

$$\vec{F}_{ij}^D = -\zeta(r_{ij}) \overleftrightarrow{P}_{ij}(\vec{r}_{ij}) \vec{v}_{ij}$$

and

$$\vec{F}_{ij}^R = \sigma(r_{ij}) \overleftrightarrow{P}_{ij}(\vec{r}_{ij}) \vec{\theta}_{ij}$$

# Choice of the projector

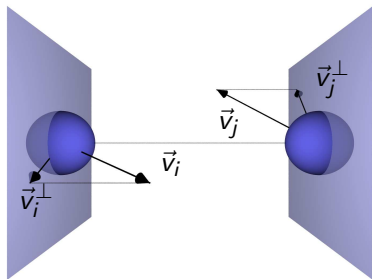
## Interesting cases

- Standard DPD

$$\overleftrightarrow{P}_{ij} = \hat{r}_{ij} \otimes \hat{r}_{ij}$$

- Transverse DPD

$$\overleftrightarrow{P}_{ij} = \overleftrightarrow{I} - \hat{r}_{ij} \otimes \hat{r}_{ij}$$



# Focker-Planck-Equation and Temperature

Controlling  
material  
properties

Christoph  
Junghans

Motivation

Introduction

DPD  
Thermostat

Simulations

Conclusion

Study of the Focker-Planck-Equation leads to:

Fluctuation-dissipation theorem

$$\sigma(r)^2 = \zeta(r)k_B T$$

We chose:

Weighting function

$$\zeta(r) = \zeta \Theta(r - r_{\text{cutoff}})$$



# Lennard-Jones fluid

## Setup

Controlling  
material  
properties

Christoph  
Junghans

Motivation

Introduction

DPD  
Thermostat

Simulations

Conclusion

- 4000 particles
- Purely repulsive Lennard-Jones interaction

$$U_{\text{LJ}} = 4\epsilon \left( \frac{1}{r^{12}} - \frac{1}{r^6} + \frac{1}{4} \right)$$

- $r_{\text{cutoff}} = 2^{1/6}$
- Different DPD thermostats at  $T_{\text{input}} = 1.2$
- $\rho_N = N/V = 0.8638$
- Varying friction strength  $\zeta$  and thermostats



# Lennard-Jones fluid

Controlling  
material  
properties

Christoph  
Junghans

Motivation

Introduction

DPD  
Thermostat

Simulations

Conclusion

## Basic observables

- Temperature

$$T = \frac{2E_{\text{kin}}}{3N_{\text{part}}} = 1.2 \pm 0.01$$

- Pressure

$$p = 9.8 \pm 0.2$$

- Radial distribution function ✓

# Lennard-Jones fluid

Diffusion constant

Controlling  
material  
properties

Christoph  
Junghans

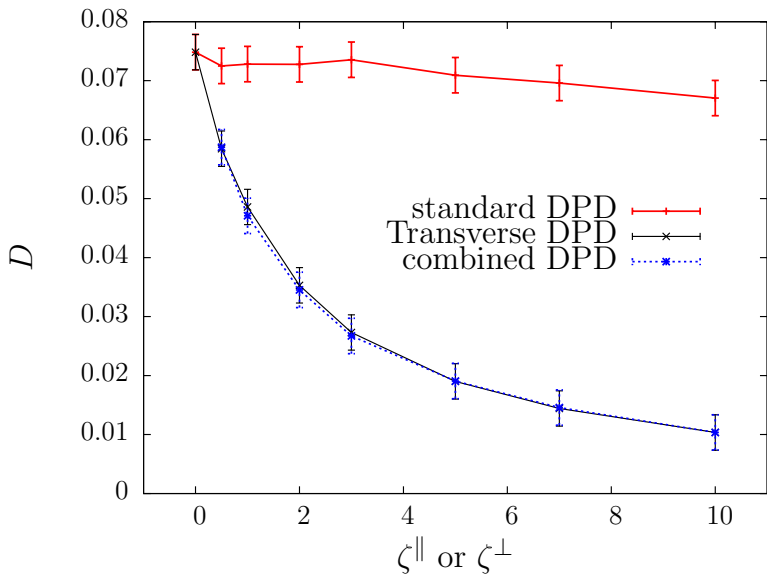
Motivation

Introduction

DPD  
Thermostat

Simulations

Conclusion



# Lennard-Jones fluid

## Viscosity

Controlling  
material  
properties

Christoph  
Junghans

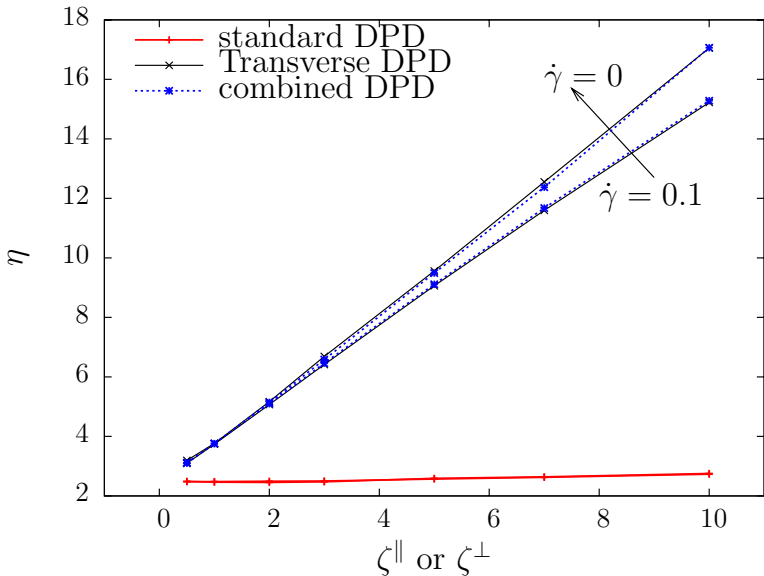
Motivation

Introduction

DPD  
Thermostat

Simulations

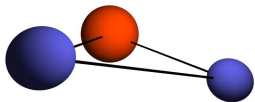
Conclusion



# TIP3P water and coarse-grained water

## Setup

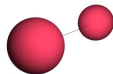
### TIP3P water model



Rigid bonds

$$\zeta^{\parallel} = 0.038\text{ps}^{-1}$$
$$\zeta^{\perp} = 0.000\text{ps}^{-1}$$

### Coarse-grained model



Tabulated potential

$$\zeta^{\parallel} = 0.00\text{ps}^{-1}$$
$$\zeta_1^{\perp} = 0.50\text{ps}^{-1}$$
$$\zeta_2^{\perp} = 0.75\text{ps}^{-1}$$
$$\zeta_3^{\perp} = 1.00\text{ps}^{-1}$$

Controlling  
material  
properties

Christoph  
Junghans

Motivation

Introduction

DPD  
Thermostat

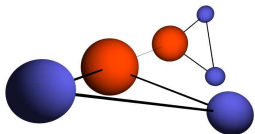
Simulations

Conclusion

# TIP3P water and coarse-grained water

## Setup

### TIP3P water model

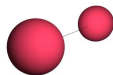


Lennard-Jones

$$\zeta^{\parallel} = 0.038\text{ps}^{-1}$$

$$\zeta^{\perp} = 0.000\text{ps}^{-1}$$

### Coarse-grained model



Tabulated potential

$$\zeta^{\parallel} = 0.00\text{ps}^{-1}$$

$$\zeta_1^{\perp} = 0.50\text{ps}^{-1}$$

$$\zeta_2^{\perp} = 0.75\text{ps}^{-1}$$

$$\zeta_3^{\perp} = 1.00\text{ps}^{-1}$$

Controlling  
material  
properties

Christoph  
Junghans

Motivation

Introduction

DPD  
Thermostat

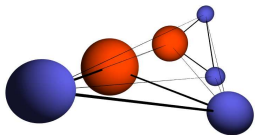
Simulations

Conclusion

# TIP3P water and coarse-grained water

## Setup

### TIP3P water model

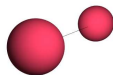


Coulomb

$$\zeta^{\parallel} = 0.038\text{ps}^{-1}$$

$$\zeta^{\perp} = 0.000\text{ps}^{-1}$$

### Coarse-grained model



Tabulated potential

$$\zeta^{\parallel} = 0.00\text{ps}^{-1}$$

$$\zeta_1^{\perp} = 0.50\text{ps}^{-1}$$

$$\zeta_2^{\perp} = 0.75\text{ps}^{-1}$$

$$\zeta_3^{\perp} = 1.00\text{ps}^{-1}$$

Controlling  
material  
properties

Christoph  
Junghans

Motivation

Introduction

DPD  
Thermostat

Simulations

Conclusion

# TIP3P water and coarse-grained water

## RDF

Controlling  
material  
properties

Christoph  
Junghans

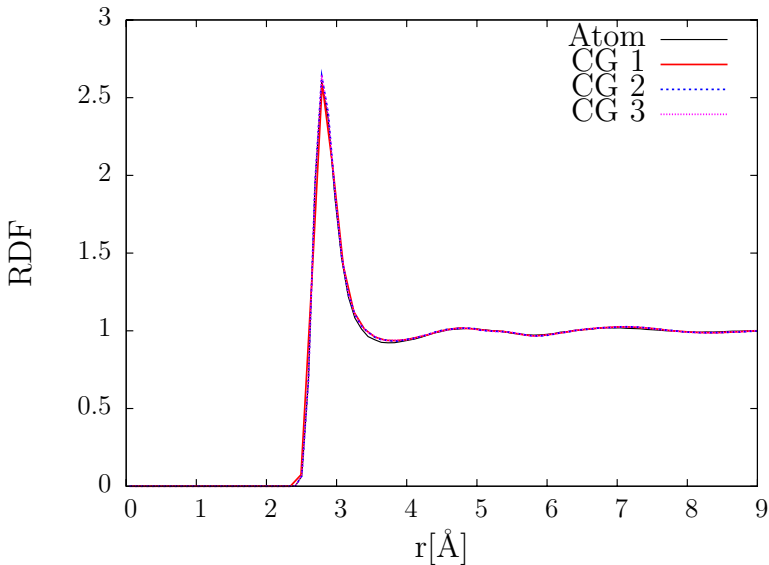
Motivation

Introduction

DPD  
Thermostat

Simulations

Conclusion



# TIP3P water and coarse-grained water

Diffusion constant

Controlling  
material  
properties

Christoph  
Junghans

Motivation

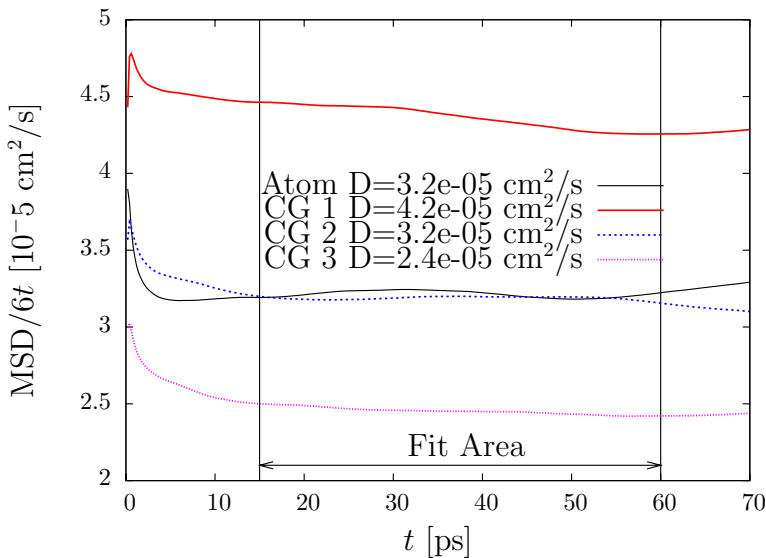
Introduction

DPD

Thermostat

Simulations

Conclusion



# TIP3P water and coarse-grained water

Controlling  
material  
properties

Christoph  
Junghans

Motivation

Introduction

DPD  
Thermostat

Simulations

Conclusion

## Other observables

- Temperature

$$T = \frac{2E_{\text{kin}}}{3N_{\text{part}}} = 300 \pm 0.5\text{K}$$

- Diffusion constant ( $D = 3.2\text{cm}^2/\text{s}$ ) matches at:

$$\zeta^{\perp} = 0.75\text{ps}^{-1}$$

- Viscosity ( $\eta = 0.5 \cdot 10^{-3}\text{Pa} \cdot \text{s}$ ) matches at:

$$\zeta^{\perp} = 0.6\text{ps}^{-1}$$



# Conclusion

Controlling  
material  
properties

Christoph  
Junghans

Motivation

Introduction

DPD  
Thermostat

Simulations

Conclusion

- Simple method to tune timescale of NVT simulations
- Analytical studies with Mori-Zwanzig formalisms show similar behaviour
- Extension to mass dependent version
- Implemented in ESPResSo package<sup>3</sup>
- Further details see: “*Transport properties controlled by a thermostat: An extended dissipative particle dynamics thermostat*”<sup>4</sup>

---

<sup>3</sup>[www.espresso.mpg.de](http://www.espresso.mpg.de)

<sup>4</sup>CJ, M. Praprotnik and K. Kremer, *Soft Matter* (2008)



# The End

Controlling  
material  
properties

Christoph  
Junghans

Thank you for your attention !